3.0 Switched Mode Power Supplies

Introduction

Switched Mode Power Supplies, (often abbreviated to SMPS) are considerably more complex than the linear regulated power supplies described in Power Supplies Module 2. The main advantage of this added complexity is that switched mode operation gives regulated DC supplies that can deliver more power for a given size, cost and weight of power unit.

Switched Mode Designs

A number of different design types are used. Where the input is the AC mains (line) supply the AC is rectified and smoothed by a reservoir capacitor before being processed by what is in effect a DC to DC converter, to produce a regulated DC output at the required level. Hence a SMPS can be used as an AC to DC converter, for use in many mains powered circuits, or DC to DC, either stepping the DC voltage up or down as required, in battery powered systems.

What you’ll learn in Module 2

Section 3.0 SMPS Introduction.
• Switch Mode Topologies.
• Stages in a Switched Mode Power Supply.
• Voltage Regulation.
• High Frequency Switching.

Section 3.1 Buck Converters.
• The Switching Transistor
• The Flywheel Circuit
• Buck Converter Operation

Section 3.2 Boost Converters.
• Boost Converter Operation.
• I.C Boost Converters.
• Output Voltage Range of Boost Converters.

Section 3.3 Buck-Boost Converters.
• Advantages of Buck-Boost Converters.
• Buck-Boost Converter Operation.

Section 3.4 Push-Pull SMPS.
• Push-Pull Switching.
• Pulse Width Modulation.
• Voltage and Current Limiting.

Section 3.4 SMPS Quiz.
• Test your knowledge of Switched Mode Power Supplies

Fig. 3.0.1 Typical SMPS Block Diagram
Switched Mode Block Diagram

Fig. 3.0.1 shows a block diagram example of a typical SMPS with an AC Mains (line) input and a regulated DC output. The output rectification and filter are isolated from the High Frequency switching section by a high frequency transformer, and voltage control feedback is via an opto isolator. The control circuit block is typical of specialist ICs containing the high frequency oscillator, pulse width modulation, voltage and current control and output shut down sections.

Whatever the purpose of a SMPS, a common feature (after conversion of AC to DC if required) is the use of a high frequency square wave to drive an electronic power switching circuit. This circuit is used to convert the DC supply into high frequency, high current AC, which by various means, depending on the design of the circuit, is reconverted into a regulated DC output. The reason for this double conversion process is that, by changing the DC or mains frequency AC to a high frequency AC, the components, such as transformers, inductors and capacitors, needed for conversion back to a regulated DC supply, can be much smaller and cheaper than those needed to do the same job at mains (line) frequency.

The high frequency AC produced during the conversion process is a square wave, which provides a means of controlling the output voltage by means of pulse width modulation. This allows the regulation of the output to be much more efficient than is possible in linear regulated supplies.

The combination of a square wave oscillator and switch used in switched mode supplies can also be used to convert DC to AC. In this way the switched mode technique also be used as an ‘inverter’ to create an AC supply at mains potential from DC supplies such as batteries, solar panels etc.

Voltage Regulation

In most switched mode supplies, regulation of both line (input voltage) and load (output voltage) is normally provided. This is achieved by altering the mark to space ratio of the oscillator waveform before applying it to the switches. Control of the mark to space ratio is achieved by comparing voltage feedback from the output of the supply with a stable reference voltage. By using this feedback to control the mark to space ratio of the oscillator, the duty cycle and therefore the average DC output of the circuit can be controlled. In this way, protection from both over voltage and over current may be provided.

Where it is important to maintain electrical isolation from the mains supply, this is provided by using a transformer, either at the AC input where it may also be used to alter the AC voltage prior to rectification, or between the control section of the power supply and the output section where, as well as providing isolation, a transformer with multiple secondary windings can produce several different voltage outputs.

To provide a well-regulated output, a sample of the DC output voltage is normally fed back to the control circuitry and compared with a stable reference voltage. Any error produced is used to control the output voltage. To maintain electrical isolation between input and output, feedback will usually be via a device such as an opto-isolator.
HF Switching

Using high frequency for the switching drive gives several advantages:

- The transformer will be of a HF type, which is much smaller than a standard mains transformer.

- The ripple frequency will be much higher (e.g. 100kHz) than in a linear supply, and so it needs a smaller value of smoothing capacitor.

- Also using a square wave to drive the switching transistors (switched mode operation) ensures that they dissipate much less power than a conventional series regulator transistor. Again this means that, for a given amount of power output, smaller and cheaper transistors can be used, than in similarly rated linear power supplies.

- The use of smaller transformers and smoothing capacitors makes switched mode power supplies lighter and less bulky. The added cost of the complex control circuitry is also offset by the smaller, and therefore cheaper transformers and smoothing capacitors, making some switched mode designs less expensive than equivalent linear supplies.

Although linear supplies can provide better regulation and better ripple rejection at low power levels than switched mode supplies, the above advantages make the SMPS the most common choice for power supply units in any equipment where a stabilised supply is needed to deliver medium to large amounts of power.

A disadvantage of using such a high frequency square wave in a powerful circuit such as a SMPS is that many powerful high frequency harmonics are created, so that without very effective RF screening and filtering, there is a danger of the SMPS creating RF interference.
3.1 Buck Converters

The Buck Converter

The Buck Converter is used in SMPS circuits where the DC output voltage needs to be lower than the DC input voltage. The DC input can be derived from rectified AC or from any DC supply. It is useful where electrical isolation is not needed between the switching circuit and the output, but where the input is from a rectified AC source, isolation between the AC source and the rectifier could be provided by a mains isolating transformer.

The switching transistor between the input and output of the Buck Converter continually switches on and off at high frequency. To maintain a continuous output, the circuit uses the energy stored in the inductor L, during the on periods of the switching transistor, to continue supplying the load during the off periods. The circuit operation depends on what is sometimes also called a Flywheel Circuit. This is because the circuit acts rather like a mechanical flywheel that, given regularly spaced pulses of energy keeps spinning smoothly (outputting energy) at a steady rate.

AC or DC Input

The buck converter is a form of DC to DC converter that can take an input directly from a DC source, such as a battery. The input could also be DC derived from the AC mains (line) as shown in Fig. 3.1.1 via a rectifier/reservoir capacitor circuit. The AC input to the rectifier circuit could be AC at high voltage directly from the AC mains supply, or alternatively at a lower voltage via a step down transformer. However the DC applied to the Buck Converter is obtained, it is then converted to a high frequency AC, using a switching or ‘chopper’ transistor, driven by a (usually pulse width modulated) square wave. This results in a high frequency AC wave, which can then be re-converted to DC in a much more efficient manner than would be possible in the circuits described in Power Supplies Module 1.

Buck Converter Operation

As shown in Fig. 3.1.1 the buck Converter circuit consists of the switching transistor, together with the flywheel circuit (D1, L1 and C1). While the transistor is on, current is flowing through the load via the inductor L1. The action of any inductor opposes changes in current flow and also acts as a store of energy. In this case the switching transistor output is prevented from increasing immediately to its peak value as the inductor stores energy taken from the increasing output; this stored energy is later released back into the circuit as a back e.m.f. as current from the switching transistor is rapidly switched off.

What you’ll learn in Module 3.1

After studying this section, you should be able to:

Understand the principles of Buck Converters.

• The Switching Transistor.

• The flywheel circuit.

Recognise the limitations on the output voltage.

Recognise different input sources.

Understand the relationship between switching pulse width and output voltage.
Transistor Switch ‘on’ Period

In Fig. 3.1.2 therefore, when the switching transistor is switched on, it is supplying the load with current. Initially current flow to the load is restricted as energy is also being stored in L1, therefore the current in the load and the charge on C1 builds up gradually during the ‘on’ period. Notice that throughout the on period, there will be a large positive voltage on D1 cathode and so the diode will be reverse biased and therefore play no part in the action.

Transistor Switch ‘off’ Period

When the transistor switches off as shown in Fig 3.1.3 the energy stored in the magnetic field around L1 is released back into the circuit. The voltage across the inductor (the back e.m.f.) is now in reverse polarity to the voltage across L1 during the ‘on’ period, and sufficient stored energy is available in the collapsing magnetic field to keep current flowing for at least part of the time the transistor switch is open.

The back e.m.f. from L1 now causes current to flow around the circuit via the load and D1, which is now forward biased. Once the inductor has returned a large part of its stored energy to the circuit and the load voltage begins to fall, the charge stored in C1 becomes the main source of current, keeping current flowing through the load until the next ‘on’ period begins.

The overall effect of this is that, instead of a large square wave appearing across the load, there remains only a ripple waveform, i.e. a small amplitude, high frequency triangular wave with a DC level of:

\[ V_{OUT} = V_{IN} \times (\text{On time of switching waveform } (t_{ON}) / \text{periodic time of switching waveform (T)}) \]

or:

\[ V_{OUT} = V_{IN} \times \frac{t_{ON}}{T} \]

Therefore if the switching waveform has a mark to space ratio of 1:1, the output \( V_{OUT} \) from the buck Converter circuit will be \( V_{IN} \times (0.5/1) \) or half of \( V_{IN} \). However if the mark to space ratio of the switching waveform is varied, any output voltage between approximately 0V and \( V_{IN} \) is possible.

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Buck Converter for Negative Supplies

For negative supplies the circuit shown in Fig. 3.1.4 can be used. This involves a change around in the positions of L1 and D1, and reversing the polarity of C compared to the circuit in Fig 3.1.2. This variation of the basic buck converter now inverts the positive DC input to produce a negative supply in the range of 0V to $-V_{IN}$.

When the input transistor switches off however, the magnetic field around L1 begins to collapse, and so induces a reversal of voltage across L1 that now makes the top of L1 negative with respect to 0V. At this time D1 becomes forward biased and conducts, causing the capacitor C1 to charge up producing a negative output voltage across the load. The actual value of negative output voltage will be the inverse of some fraction of the input voltage and depends on the mark to space ratio of the square wave signal applied input switch, which will be a pulse width modulated signal, typically operating at a constant frequency at tens of KHz.
3.2 Boost Converters

What you’ll learn in Module 3.2

After studying this section, you should be able to:

- Understand the principles of Boost Converters.
- The Switching Transistor
- The Flywheel Circuit
- Recognise the limitations on the output voltage.
- Recognise different input sources.
- Understand the relationship between switching pulse width and output voltage.

Boost Converter

Switched mode supplies can be used for many purposes including DC to DC converters. Often, although a DC supply, such as a battery may be available, its available voltage is not suitable for the system being supplied. For example, the motors used in driving electric automobiles require much higher voltages, in the region of 500V, than could be supplied by a battery alone. Even if banks of batteries were used, the extra weight and space taken up would be too great to be practical. The answer to this problem is to use fewer batteries and to boost the available DC voltage to the required level by using a boost converter. Another problem with batteries, large or small, is that their output voltage varies as the available charge is used up, and at some point the battery voltage becomes too low to power the circuit being supplied. However, if this low output level can be boosted back up to a useful level again, by using a boost converter, the life of the battery can be extended.

The DC input to a boost converter can be from many sources as well as batteries, such as rectified AC from the mains supply, or DC from solar panels, fuel cells, dynamos and DC generators. The boost converter is different to the Buck Converter in that it’s output voltage is equal to, or greater than its input voltage. However it is important to remember that, as power (P) = voltage (V) x current (I), if the output voltage is increased, the available output current must decrease.

Fig. 3.2.1 illustrates the basic circuit of a Boost converter. However, in this example the switching transistor is a power MOSFET, both Bipolar power transistors and MOSFETs are used in power switching, the choice being determined by the current, voltage, switching speed and cost considerations. The rest of the components are the same as those used in the buck converter illustrated in Fig. 3.1.2, except that their positions have been rearranged.

Boost converter Operation

Fig 3.2.2 illustrates the circuit action during the initial high period of the high frequency square wave applied to the MOSFET gate at start up. During this time MOSFET conducts, placing a short circuit from the right hand side of L1 to the negative input supply terminal. Therefore a current flows between the positive and negative supply terminals through L1, which stores energy in its magnetic field. There is virtually no current flowing in the remainder of the circuit as the combination of D1, C1 and the load represent a much higher impedance than the path directly through the heavily conducting MOSFET.
Fig. 3.2.3 shows the current path during the low period of the switching square wave cycle. As the MOSFET is rapidly turned off the sudden drop in current causes L1 to produce a back e.m.f. in the opposite polarity to the voltage across L1 during the on period, to keep current flowing. This results in two voltages, the supply voltage $V_{IN}$ and the back e.m.f. ($V_L$) across L1 in series with each other.

This higher voltage ($V_{IN} + V_L$), now that there is no current path through the MOSFET, forward biases D1. The resulting current through D1 charges up C1 to $V_{IN} + V_L$ minus the small forward voltage drop across D1, and also supplies the load.

Fig.3.2.4 shows the circuit action during MOSFET on periods after the initial start up. Each time the MOSFET conducts, the cathode of D1 is more positive than its anode, due to the charge on C1. D1 is therefore turned off so the output of the circuit is isolated from the input, however the load continues to be supplied with $V_{IN} + V_L$ from the charge on C1. Although the charge C1 drains away through the load during this period, C1 is recharged each time the MOSFET switches off, so maintaining an almost steady output voltage across the load.

The theoretical DC output voltage is determined by the input voltage ($V_{IN}$) divided by 1 minus the duty cycle (D) of the switching waveform, which will be some figure between 0 and 1 (corresponding to 0 to 100%) and therefore can be determined using the following formula:

**Example:**

If the switching square wave has a period of 10µs, the input voltage is 9V and the ON is half of the periodic time, i.e. 5µs, then the output voltage will be:

$$V_{OUT} = \frac{9}{1 - 0.5} = \frac{9}{0.5} = 18V \text{ (minus output diode voltage drop)}$$

Because the output voltage is dependent on the duty cycle, it is important that this is accurately controlled. For example if the duty cycle increased from 0.5 to 0.99 the output voltage produced would be:

$$V_{OUT} = \frac{9}{1 - 0.99} = \frac{9}{0.01} = 900V$$

Before this level of output voltage was reached however, there would of course be some serious damage (and smoke) caused, so in practice, unless the circuit is specifically designed for very high voltages, the changes in duty cycle are kept much lower than indicated in this example.
I.C. Boost Converter

Because of the ease with which boost converters can supply large over voltages, they will almost always include some regulation to control the output voltage, and there are many I.C.s manufactured for this purpose. A typical example of an I.C. boost converter is shown in Fig. 3.2.6, in this example the LM27313 from Texas Instruments. This chip is designed for use in low power systems such as PDAs, cameras, mobile phones, and GPS devices.

In this circuit, an appropriate fraction of the output voltage \( V_{OUT} \), dependent on the ratio of \( R2:R3 \) is used as a sample and compared with a reference voltage within the I.C. This produces an error voltage that is used to alter the duty cycle of the switching oscillator, enabling a range of automatically regulated boost voltages between 5V and 28V to be obtained.

The LM27313 contains an internal oscillator operating at a fixed frequency of about 1.6MHz. The FET switching transistor is also internal and switches the current through \( L1 \) via the SW terminal. Notice also that a Schottky diode with an appropriate voltage and current rating is used for \( D1 \) to keep losses due to the forward voltage drop of the diode as small as possible, and to enable high switching speeds to be achieved. The I.C. also has a shut down (SHDN) facility, operated by external logic, by which the boost converter may be disabled when not required, to save battery power.

Protection Circuits

Other safety features provided by the I.C. are over current shut down, which disables the switch on a cycle-by-cycle basis if too much current is sensed, and an over temperature shut down facility.

Stability

Another problem facing designers of high frequency boost converters is that of stability, as at MHz frequencies both negative and positive feedback can occur simply due to electromagnetic fields radiating between components within the circuit, especially where the circuit components are in very close proximity as in surface mount layouts. \( C2 \) is therefore added to improve stability and prevent possible oscillation due to unwanted positive feedback occurring.
3.3 Buck-Boost Converters

What you’ll learn in Module 3.3

After studying this section, you should be able to:

- Understand the need for a choice of DC to DC converter designs.
- Understand the principles of Buck-Boost Converters.
  - The switching transistors.
  - Switching control systems.
- Understand the relationships between different converter designs.
  - Buck converters.
  - Boost converters.
  - Buck-Boost converters.
- Recognise the limitations on the output voltage.
- Recognise typical commercial I.Cs. using buck boost technology.

Buck-Boost Converters

A Buck-Boost converter is a type of switched mode power supply that combines the principles of the Buck Converter and the Boost converter in a single circuit. Like other SMPS designs, it provides a regulated DC output voltage from either an AC or a DC input.

The Buck converter described in Power Supplies Module 3.1 produces a DC output in a range from 0V to just less than the input voltage. The boost converter will produce an output voltage ranging from the same voltage as the input, to a level much higher than the input.

There are many applications however, such as battery-powered systems, where the input voltage can vary widely, starting at full charge and gradually decreasing as the battery charge is used up. At full charge, where the battery voltage may be higher than actually needed by the circuit being powered, a buck regulator would be ideal to keep the supply voltage steady. However as the charge diminishes the input voltage falls below the level required by the circuit, and either the battery must be discarded or re-charged; at this point the ideal alternative would be the boost regulator described in Power Supplies Module 3.2.

By combining these two regulator designs it is possible to have a regulator circuit that can cope with a wide range of input voltages both higher or lower than that needed by the circuit. Fortunately both buck and boost converters use very similar components; they just need to be re-arranged, depending on the level of the input voltage.

In Fig. 3.3.1 the common components of the buck and boost circuits are combined. A control unit is added, which senses the level of input voltage, then selects the appropriate circuit action. (Note that in the examples in this section the transistors are shown as MOSFETs, commonly used in high frequency power converters, and the diodes shown as Schottky types. These diodes have a low forward junction voltage when conducting, and are able to switch at high speeds).
Operation as a Buck Converter

The basic operation of the buck boost converter is illustrated in Figs. 3.3.2 to 3.3.5

Fig. 3.3.2 shows the circuit operating as a Buck Converter. In this mode Tr2 is turned off, and Tr1 is switched on and off by a high frequency square wave from the control unit. When the gate of Tr1 is high, current flows though L, charging its magnetic field, charging C and supplying the load. The Schottky diode D1 is turned off due to the positive voltage on its cathode.

Fig 3.3.3 shows the current flow during the buck operation of the circuit when the control unit switches Tr1 off. The initial source of current is now the inductor L. Its magnetic field is collapsing, the back e.m.f. generated by the collapsing field reverses the polarity of the voltage across L, which turns on D1 and current flows through D2 and the load.

As the current due to the discharge of L decreases, the charge accumulated in C during the on period of Tr1 now also adds to the current flowing through the load, keeping \( V_{\text{OUT}} \) reasonably constant during the off period. This helps keep the ripple amplitude to a minimum and \( V_{\text{OUT}} \) close to the value of \( V_S \).

Operation as a Boost Converter

In Boost Converter mode, Tr1 is turned on continually and the high frequency square wave applied to Tr2 gate. During the on periods when Tr2 is conducting, the input current flows through the inductor L and via Tr2, directly back to the supply negative terminal charging up the magnetic field around L. Whilst this is happening D2 cannot conduct as its anode is being held at ground potential by the heavily conducting Tr2.

For the duration of the on period, the load is being supplied entirely by the charge on the capacitor C, built up on previous oscillator cycles. The gradual discharge of C during the on period (and its subsequent recharging) accounts for the amount of high frequency ripple on the output voltage, which is at a potential of approximately \( V_S + V_L \).

(Contd.)
The Off Period

At the start of the off period of Tr2, L is charged and C is partially discharged. The inductor L now generates a back e.m.f. and its value that depends on the rate of change of current as Tr2 switches off and on the amount of inductance the coil possesses; therefore the back e.m.f can be any voltage over a wide range, depending on the design of the circuit. Notice particularly that the polarity of the voltage across L has now reversed, and so adds to the input voltage $V_S$ giving an output voltage that is at least equal to or greater than the input voltage. D2 is now forward biased and so the circuit current supplies the load current, and at the same time re-charges the capacitor to $V_S + V_L$ ready for the next on period of Tr2.

Circuit Variations

There are a number of variations of this basic Buck-Boost circuit, some designs working at lower frequencies or at high voltages may use bipolar transistors instead of MOSFETs; at low frequencies the higher speed switching of MOSFETs is less of an advantage. Also, in high voltage designs, silicon diodes may be used in preference to Schottky types due to the silicon diode’s higher reverse voltage capabilities. Another variation is to use synchronous switching where, instead of using diodes that simply respond to the voltage polarity across them, four synchronised (by the control unit) MOSFETs do all the switching.

The control unit may also carry out over current and over voltage protection, as well as the normal oscillator and pulse width modulation functions to regulate the output voltage.

Another commonly used facility is ‘pulse skipping’ where the control unit prevents charging on one or more oscillator pulses when it senses that the load current is low. This reduces the overall current drawn from the (typically battery) supply, prolonging battery life.

Buck-Boost Converter I.Cs. are commonly used to carry out the control unit functions. These range from very low power, high efficiency I.Cs. for portable devices such as mobile phones and automotive applications, such as the TPS63000 series from Texas Instruments, and the LTC3789 from Linear Technology, to large industrial high power DC-DC converters providing many kilowatts of output power.
3.4 Push-Pull Switched Mode Power Supplies

What you'll learn in Module 3.4

After studying this section, you should be able to:

Understand the operation of a push pull DC to DC converter.

Understand the operation of a typical switch mode controller I.C.

- Power switching transistors.
- Pulse width modulator.
- Over current & over voltage protection.
- Current sensing.

Recognise components and methods used for output isolation.

The Push Pull SMPS

Fig. 3.4.1 shows a block diagram of a switched mode power supply designed around a UC3524 Advanced Regulating Pulse Width Modulator by Texas Instruments.

The circuit is a DC to DC converter using a DC input voltage of 15V to 30V and produces a regulated 5V output at a current up to about 250mA. The circuit uses push pull power switching driving a high frequency transformer, which fully isolates the output circuit from the input. The output is short circuit protected, and the output voltage can be manually adjusted. Maximum current can be also manually set using adjustable current limiting.

Primary Circuit.

A 100kHz oscillator within IC1 (UC3524) generates pulses, which are processed by the pulse width modulator (within IC1) used to drive the power switching transistors. The width of the processed drive pulses controls the length of time for which the power switching transistors conduct, and therefore the amount of power delivered to the transformer.

The pulse width and therefore the output voltage are controlled by the error amplifier in IC1. This measures the difference between a sample of the output voltage, fed back via the opto-isolator, and a reference voltage set by Vr1. When these two voltages are equal, the circuit output voltage is correct. If there is a difference, the width of the pulses produced by the pulse width modulator is increased or decreased to correct the error.

Over current protection is provided to ensure that the supply is shut down in the event of too high a current demand at the output. The output terminals can even be shorted together without damaging the supply.

Each pulse of current in the power switching transistors produces a voltage pulse across the sensing resistor R12. The amplitude of these pulses is proportional to the current being delivered to the transformer by the switching circuit. If the peak value of any of these pulses exceeds the DC voltage set by Vr2 (Current limit) then the output from IC2 will cause pulse width modulator input to reduce the width of the pulse being produced by the modulator at that time, momentarily reducing the output voltage. If the over current condition disappears, the output voltage will be restored to its normal level, but if the load current remains high, the current limiter will continue to reduce the output.
pulse width, dependent on the amount of over current, even down to zero in the case of a short circuit output.

**The Secondary Circuit**

The push pull switching transistors create an AC waveform across the transformer primary winding, and the secondary winding feeds a conventional full wave rectifier and LC low pass filter to supply the load with a stable 5V at the output terminals. Negative feedback to the voltage regulating circuit in IC1 is via the opto-isolator (IC3). The higher the output voltage, the brighter the glow from an LED sealed within the secondary side, and the larger the DC output voltage derived from pin 4 of IC3 in the primary side of the device. This voltage is used as a sample at the inverting input of the error amplifier in IC1 where it is compared with a voltage from the ‘set voltage’ control VR1, to control the pulse width modulator.

**Circuit Description**

The full schematic diagram for the circuit is shown in Fig. 3.4.2.

![Fig. 3.4.2 Circuit diagram of a push-pull SMPS using the Texas Instruments UC3524 I.C.](image)

The oscillator within IC1 produces narrow 100kHz (approx) pulses that are used as clock pulses for the Switch Logic within IC1. The timing components for the oscillator are R3 and C2. The ramp waveform produced as C2 charges is also used as an input to the inverting input of the comparator in IC1. The pulse width modulator comprises the comparator within IC1 and the switching logic, which consists of a bistable and two three input NOR gates. The outputs of this block supply variable width pulses to the two transistors Qa and Qb.
The error amplifier compares a stable reference voltage on pin 1 (set by Vr1 supplied from an internally regulated 5V from pin 16) with a sample of the load voltage developed across the opto-isolator emitter resistor, R11. The resulting error voltage is used as the non-inverting input to the PWM comparator.

The facilities of the UC3524 that are used in this circuit are shown in more detail in Fig. 3.4.3 (Note: Some unused facilities of the UC3524 have been omitted for clarity, for more information see the Texas Instruments UC3524 data sheet).

**Pulse Width Modulator**

The action of the pulse width modulator, described by the waveforms shown in Fig. 3.4.4 is as follows:

Clock pulses (CK) from the oscillator are fed to the Bi-stable (flip-flop), which produces a square wave with a 1:1 mark/space ratio and a frequency of 50kHz, (half that of the oscillator) at its Q output, and an inverted version of this wave at its $\overline{Q}$ output.

Output Q provides an input to NOR gate a, and output $\overline{Q}$ (the opposite of Q) provides an input to NOR gates b. The logic rule for a NOR gate is that its output will be high, only when all its three inputs are low. Notice that the Q and $\overline{Q}$ signals go low at the start of alternate clock pulse low states. The clock signal also provides an input to both NOR gates.

The third input to each of the NOR gates is provided by the comparator output, which is a series of variable width low state pulses, produced by comparing the DC error voltage from the error amplifier in IC1 with the ramp produced by the oscillator timing capacitor C2.

As each NOR gate output goes high, only when all of its three input signals are low, alternate high state pulses, whose width depends on the value of the error voltage, are fed to the bases of the internal transistors Qa and Qb. The lower the value of the error voltage (due to a higher value of "sample" voltage at pin 1) the narrower the pulses produced. These narrower pulses, when used to turn on the power switching transistors TR3 and Tr4, will lead to a reduction in power in the transformer and a reduction in load voltage.
Power Switching Circuits

The internal drive transistors Qa and Qb each produces a series of pulses at its collector, and an a series of anti-phase pulses at its emitter. The emitter signals a and b drive the power switching transistors Tr3 and Tr4 respectively, and the collector signals drive the speed up circuits Tr1/Tr2.

The reason for including the speed up circuits is to overcome the delay that would normally happen because while the power switching transistors Tr3 and Tr4 are conducting, their base/emitter junction (which naturally forms a small capacitor due to the depletion layer between the base and emitter layers in the transistor) is charged up, and must be discharged before the transistor will fully turn off.

The power transistor junctions are rapidly discharged by momentarily turning on Tr1 or Tr2 using a differentiated pulse generated from the rising edge of the waveform from the collector of Qa or Qb in IC1, which of course happens at exactly the same instant as Tr3 or Tr4 is turning off, as illustrated in Fig 3.4.5.

Because the transformer primary centre tap is connected to the main (+VIN) supply, it will always be at the supply potential. The collector voltages of Tr3 and Tr4 will also be at +VIN during the periods when both transistors are turned off.

During the ‘on’ pulse of Tr3, its collector will be at approximately 0V, and due to the centre tapping of the transformer primary winding the bottom half of the primary will be in anti-phase to the top half, so the collector of Tr4 will be positive at twice the value of +VIN for the period of the Tr3 ‘on’ pulse. This situation is reversed during the ‘on’ pulse of Tr4. This action produces a stepped type of waveform with an amplitude of +VIN x 2 across the transformer primary as shown in Fig 3.4.4.

The Secondary Circuit

The resulting secondary voltage is rectified by D1 and D2, and smoothed by the low pass filter L1/C10 before being supplied to the load. A sample of the load voltage is fed back to the LED within opto-isolator IC3 via the LED current limiting resistor R13.
Because of the push pull design used by this circuit, it is a simple matter to arrange for such a circuit to have multiple outputs. Different (higher or lower) voltages can be obtained by using a transformer similar to the one illustrated in Fig. 3.4.6, which has multiple secondary windings with appropriate turns ratios.

The total current supplied to the multiple outputs however, must not exceed the maximum current rating of the SMPS. Each supply line will have its own rectifier and filter system, and may also include some extra point of load regulation. A voltage sample will normally be taken from only one of the outputs to provide feedback to the pulse width modulator however, as controlling the power applied to the transformer primary will control all the voltage outputs.

**Current limiting**

Current limiting, which is capable of completely shutting down the circuit under extreme overload conditions is provided by the action of IC2 and the shut down transistor between pins 9 and 10 within IC1.

Pin 3 of IC2 is provided with a stable reference voltage derived from the shunt voltage regulator R7/ZD1 via the current limit control Vr2. The non-inverting input of IC2 is connected to a low resistance current sensing resistor R12 in the emitter lead common to both switching transistors Tr3/Tr4.

Every time either transistor conducts, the resulting large emitter current produces a voltage pulse across R12. The peak voltage of this pulse will be proportional to the emitter current flowing in Tr3/Tr4 and therefore, also to the output current.

If the peak voltage of any of these pulses applied to the non-inverting input of IC2 exceeds the stabilised DC voltage at the inverting input, a positive pulse will be produced at the output, and therefore at the base of Qc within IC1. This will cause the collector voltage of this transistor to fall, also reducing the error amplifier output that is controlling the pulse width modulator. This action has the effect of reducing the width of the pulse presently being produced, thus instantly reducing output voltage. If the current overload disappears, the pulse width modulator will return to normal operation. If not, subsequent pulses will be further reduced until the output voltage falls (if necessary) to zero.

The action of the current limit circuit is not absolutely instant however, due to the presence of C4 on the shut down compensation pin (9) of IC1. This capacitor tends to integrate the voltage changes on the collector of the shut down transistor so that very rapid (cycle by cycle) variations of the output voltage during current limiter action are avoided.
3.5 Switched Mode Power Supplies Quiz

Try our quiz, based on the information you can find in Power Supplies Module 3. Check your answers at http://www.learnabout-electronics.org/PSU/psu35.php and see how many you get right. If you get any answers wrong, just follow the hints to find the right answer, and learn about Switched Mode Power Supplies as you go.

1. Which answer from the following list is a major advantage of switched mode power supplies over series regulated supplies?
   a) Switched mode supplies create smaller amplitude ripple waveforms than series regulators.
   b) Switched mode supplies dissipate less power in the control element than series regulators.
   c) Switched mode supplies provide better regulation at low power than series regulators.
   d) Switched mode supplies work digitally, so are more efficient than series regulators.

2. Which answer from the following list is a disadvantage of switched mode power supplies compared with series regulated supplies?
   a) Switched mode supplies are less suitable for high power applications.
   b) Switched mode supplies are more expensive to implement than series regulated supplies.
   c) It is more difficult to prevent high frequency electrical interference in switched mode supplies.
   d) Over voltage protection is not possible in switched mode power supplies.

3. Which one of the following acts as an energy store in a DC to DC Converter?
   a) The inductor.
   b) The high frequency switching transistor.
   c) The load.
   d) The flywheel diode.

4. Refer to Fig 3.5.1. Which of the following components is not active during the ON period of the switching waveform?
   a) Tr1
   b) D1
   c) L1
   d) C2

5. What type of circuit is illustrated in Fig 3.5.2?
   a) Buck Converter.
   b) Boost Converter.
   c) Buck-boost Converter.
   d) Flyback Converter
6. Which of the following is one of the main advantages of a push-pull converter compared to buck or boost DC to DC converters?

a) It works at twice the frequency of other DC to DC converters.

b) It uses pulse width modulation.

c) It provides an output voltage of twice the amplitude of the input.

d) It uses a transformer to isolate the output from the input.

7. Which of the following statements is true of a Buck-Boost Converter?

a) The output power may be less than, or greater than the input power.

b) The output voltage is always greater than the input voltage.

c) The output current is always greater than the input current.

d) The output voltage may be less than, or greater than the input voltage.

8. Refer to Fig. 3.5.3. What is the purpose of Tr1 and Tr2?

a) They act with Tr3 and Tr4 to form two Darlington Pair output stages.

b) They isolate the output transistors from the common ground connection.

c) They speed up the switch off time of the output transistors.

d) They integrate the square wave signals to the bases of Tr3 and Tr4.
9. Refer to Fig. 3.5.3. What is the purpose of IC2?
   a) It acts as a comparator for the current limiter.
   b) It acts as an error amplifier for the current limiter.
   c) It acts as a comparator for the over voltage control.
   d) It acts as an error amplifier for the over voltage control.

10. Refer to Fig. 3.5.3. What type of signal will be present at pin 4 of IC3.
    a) 50kHz pulses with an amplitude proportional to the output voltage.
    b) A DC voltage proportional to the output current.
    c) 100kHz pulses with an amplitude proportional to the output current.
    d) A DC voltage proportional to the output voltage.